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**CHESAPEAKE BAY INSTITUTE
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REPORT ON SPECIAL
CORES TAKEN FOR NRL
IN THE YORK RIVER

Reference 52-6

Feb 52

CHESAPEAKE BAY INSTITUTE
THE JOHNS HOPKINS UNIVERSITY

Reference No. 52-6

REPORT ON SPECIAL CORES TAKEN IN THE YORK RIVER
FOR THE NAVAL RESEARCH LABORATORY

By

M. C. Powers

This report contains results of work carried out for the Office of Naval Research and the Hydrographic Office of the Navy Department under Contract No. Nonr-24807 with The Johns Hopkins University.

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Wayne V. Burt
Project Supervisor
February 29, 1952

PHYSICAL DATA FROM BOTTOM CORES OBTAINED
OFF PIER 1 OF THE NAVAL MINE DEPOT,
YORK RIVER

Six cores were taken at the request of NRL personnel working in conjunction with Operation MUD in the area adjacent to Pier 1 of the Naval Mine Depot at Yorktown, Virginia. The locations of the cores are shown in Figure 1. This report contains analyses of cores as requested by NRL. The results of certain other tests which were made in the field are listed.

The sediments in the area are predominantly sand which is derived chiefly from the erosion of nearby beaches. There can be little doubt but what ships occasionally stir the bottom sediments. This stirring puts sediments into suspension and probably results in occasional changes in the type material present.

Field Tests

As soon as the cores were extruded aboard ship the natural water content, wet density, rigdense and pH were determined. These tests have been described in Chesapeake Bay Institute, Inshore Survey Program, Interim Reports.

Natural water content and porosity are determined from the water contained in the sediment according to the following equations:

$$\text{Natural water} = \frac{\text{Wet weight} - \text{Dry Weight}}{\text{Dry Weight}} \times 100$$

$$\text{Porosity} = \frac{\text{Wet Weight} - \text{Dry Weight}}{\left(\frac{\text{Dry Weight}}{2.65} \right) + \text{Weight of water}} \times 100$$

In determining porosity it is assumed that the pore space in the sediments is saturated with water.

Wet density of the bulk material was measured with a Braun "MUDWATE" hydrometer.

Rigdense is the depth in centimeters to which a small penetrometer sinks in a section of the core in two minutes.

pH was determined with "pHydrion" pH paper placed directly on the core immediately after extrusion.

Laboratory Size Determinations

Size distribution determinations were run on samples taken at various depths in the cores. The samples were selected on the basis of lithologic changes in the cores.

The samples were dispersed in sodium carbonate after removing organic matter and calcium carbonate which tends to flocculate the clay and fine silt fractions. "U. S. Standard" sieves were used to separate fractions larger than 0.062 millimeters. A "BOUYOUKOS" hydrometer was used in the analysis of the lutites. These results were checked against pipette analyses. Only hydrometer results are given in this report.

Most of the central tendencies from the cumulative curves occur in the sand size fractions and are therefore reliable. However, the size analysis of particles less than about 0.03 mm is subject to error due to difference in the dis-aggregating ability of the dispersal agent used. Therefore the size analysis of the fractions in the fine silt and clay range does not give the size distributions that occur in the natural environment.

Central Tendencies and Parameters

Cumulative curves were plotted and the following parameters and central tendencies which are discussed by Krumbein and Pettijohn (Manual of Sedimentary Petrography, 1938, Chapter 9) were determined:

Md Median diameter in mm.

Q₁, Q₃ First and third quartiles.

P₁₀, P₉₀ Ten and ninety percentiles.

QD_a = $\frac{Q_3 - Q_1}{2}$ Arithmetic quartile deviation.

This last term is a measure of sorting and though rarely used by sedimentologists it may prove useful in studying the attenuation of sound through sediments since it is affected by grain size. The smaller the numerical value the better the sorting. Values greater than 0.1 are considered poorly sorted.

$$Sk_a = \frac{Q_3 + Q_1}{2} - Md \quad \text{Arithmetic quartile skewness.}$$

This measure of skewness is affected by grain size. A zero value indicates a perfectly symmetrical frequency distribution. Distributions with negative values are skewed toward larger grain sizes and those with positive values are skewed toward smaller grain sizes.

$$Kq_a = \frac{Q_3 - Q_1}{2(P_{90} - P_{10})} \quad \text{Arithmetic quartile kurtosis.}$$

The lower the numerical value, the flatter the frequency curve. The values are independent of grain size.

$$QD_g = \sqrt{\frac{Q_3}{Q_1}} \quad \text{Geometric quartile deviation.}$$

According to Trask (Origin and Environment of Source Sediments of Petroleum, 1932), who introduced this as a "sorting coefficient", values less than 2.5 indicate well sorted sediments, values from 2.5 to 4.0 indicate moderate sorting while values greater than 4.0 indicate poor sorting.

$$Sk = \frac{Q_3 - Q_1}{Md} \quad \text{Square of the geometric quartile skewness.}$$

A perfectly symmetrical frequency curve would have an Sk value of 1.0. Curves with Sk greater than 1.0 are skewed toward smaller grain size and curves with Sk less than 1.0 are skewed toward larger grain sizes.

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- V -

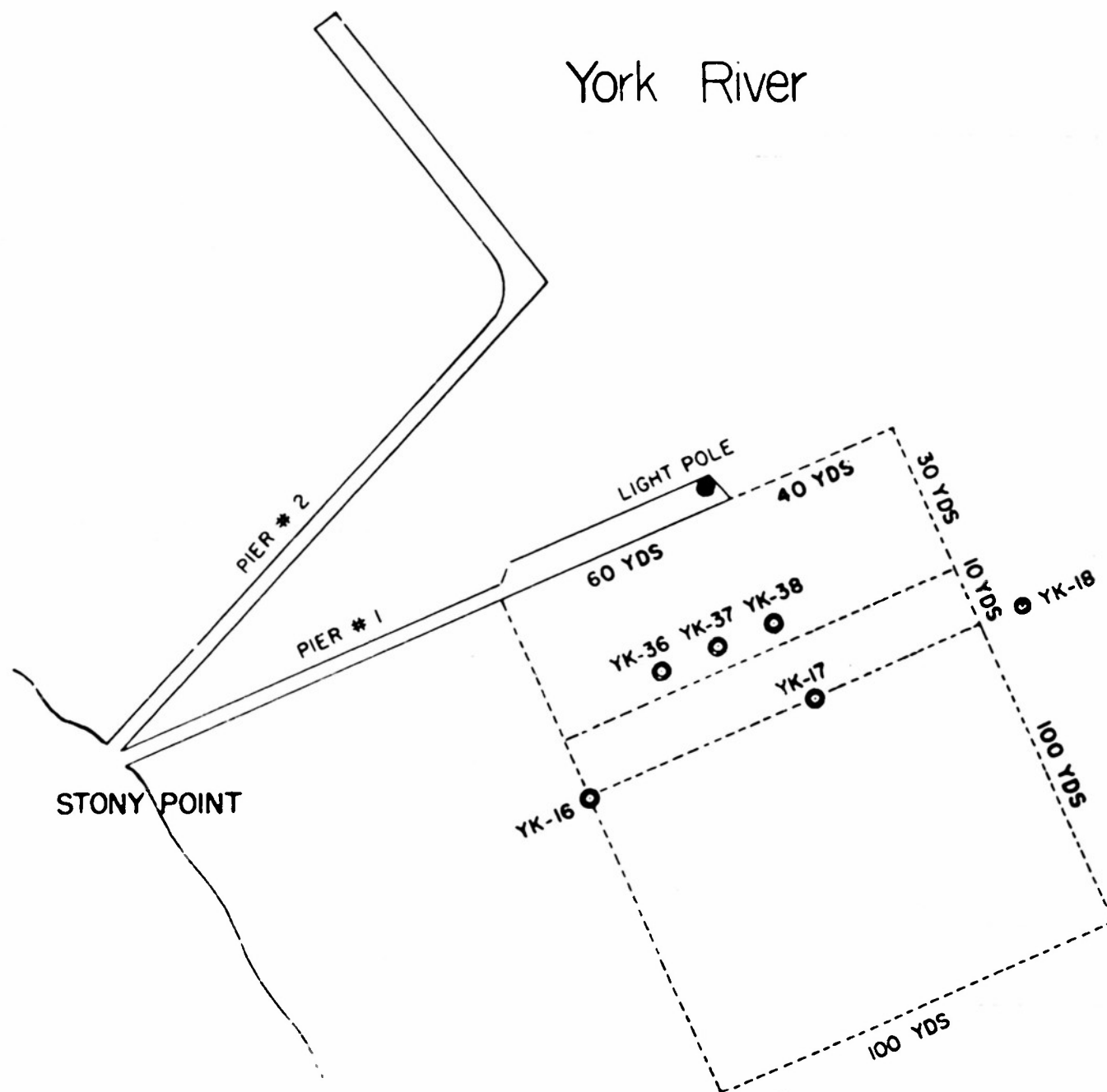


Figure 1. Chart showing location of cores.

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- 1 -

Core YK-16

Depth from top in feet	% Nat. water	% Porosity	Wet Density	Rid. value	Odor	pH
0	190.42	81.5	1.12	5.7	None	8.0
2	197.97	82.9	1.26	3.6	None	8.0
4	58.68	60.8	1.64	3.3	None	8.0
6	28.80	43.2	1.98	1.7	None	8.0
6 $\frac{1}{2}$	--	--	--	3.3	None	8.0
8	60.97	56.7	1.57	4.8	None	8.0
9 $\frac{1}{2}$	51.33	57.6	1.43	--	None	8.0

Description

Depth from top in inches	Color	Roundness *	Megascopic sorting**	Grain size of sand fraction***
0-24	black	--	W.	V. F.
24-66	dark grey	--	P.	F. to V. F.
66-74	yellow	A. to S.A.	P.	C. to F.
74-Bottom	dark grey	A. to S.A.	P.	M. to V. F.

Depth from top in inches	Estimated % of				Consistency or induration
	Gravel	sand	silt	clay	
0-24	--	30	40	30	Oozey to plastic
24-66	5	60	25	10	Plastic to almost soupy
66-74	--	90	5	5	Semi-plastic
74-Bottom	--	85	10	5	Semi-plastic

*Roundness

V. A. - Very Angular, A. - Angular, S. A. - Subangular, S. R. - Subrounded
R. - Rounded, W. R. - Well Rounded

**Megascopic Sorting

W. - Well sorted, S. - sorted, P. - Poorly sorted, V. P. - Very Poorly sorted

***Grain Size of Sand Fraction

V. F. - Very Fine, F. - Fine, M. F. - Medium Fine, Medium, C. - Coarse,
G. - Gravel

CONFIDENTIAL

- 2 -

Core YK-17

Depth from top in feet	% Nat. water	% Porosity	Wet Density	Rid. value	Odor	pH
0	139.37	78.6	1.40	5.8	None	7.0
2	33.55	47.3	1.98	3.7	None	7.0
3 $\frac{1}{2}$	24.33	39.1	1.96	2.0	None	7.0

Description

Depth from top in inches	Color	Roundness *	Megascopic sorting**	Grain size of sand fraction***
0-6	Medium grey	--	W.	F. to V. F.
6-40	Light grey	S.A. to A.	P.	C. to V. F.
40-42	Light grey	S.A. to A.	P.	Mostly C.

Depth from top in inches	Estimated % of				Consistency or induration
	Gravel	sand	silt	clay	
0-6	--	70	15	15	Oozey
6-40	--	90	5	5	Soupy
40-42	5	90	2.5	2.5	Wet

Core YK-18

Depth from top in feet	% Nat. water	% Porosity	Wet Density	Rid. value	Odor	pH
0	142.29	78.9	1.63	2.0	H ₂ S	7.5
2	137.09	78.4	1.42	0.5	H ₂ S	7.5
4	32.71	46.0	--	2.2	H ₂ S	7.5
6	102.04	73.0	--	6+	None	7.5

Description

Depth from top in inches	Color	Roundness *	Megascopic sorting**	Grain size of sand fraction***
0-18	Medium grey	--	W.	V. F.
18-48	Brown	S.A. to A.	P.	C. to V. F.
48-72	Medium grey	--	S.	V. F.

Depth from top in inches	Estimated % of				Consistency or induration
	Gravel	sand	silt	clay	
0-18	--	75	15	10	Hard-plastic
18-48	--	90	5	5	Hard-plastic
48-72	--	30	40	30	Soupy with hard-plastic clay balls

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- 3 -

Core YK-36

Depth from top in feet	% Nat. water	% Porosity	Wet Density	Rid. value	Odor	pH
0	215.00	85.0	1.25	6+	None	7.2
2	175.00	82.4	1.28	4.7	None	7.2
4	38.00	50.0	1.73	4.4	None	7.0
6	36.00	49.1	1.88	4.3	None	7.0
8	37.00	49.3	1.89	3.8	None	7.0

Description

Depth from top in inches	Color	Roundness *	Megascopic sorting**	Grain size of sand fraction***
0-30	Dark grey	S.R. to W.R. Mostly W.R.	S.	F. to V.F. Mostly M.F.
30-54	Mustard salt & pepper	R. to W.R. Mostly W.R.	S.	M. to F. Mostly M.F.
54-96	Mustard salt & pepper	R. to W.R. Mostly W.R.	W.	M. to V.F. Mostly F.

Depth from top in inches	Estimated % of				Consistency or induration
	Gravel	sand	silt	clay	
0-30	--	5	55	40	Sticky gelatinous
30-54	--	60	30	10	Soggy slick sand
54-96	--	100	--	--	Very wet squishy

Core YK-37

Depth from top in feet	% Nat. water	% Porosity	Wet Density	Rid. value	Odor	pH
0	42.00	52.5	1.83	6+	None	7.0
2½	35.00	48.4	1.90	4.7	None	7.0

Description

Depth from top in inches	Color	Roundness *	Megascopic sorting**	Grain size of sand fraction***
0-12	Medium grey salt & pepper	R. to W.R. Mostly W.R.	S.	M. to F. Mostly M.
12-30	Medium grey salt & pepper	R. to W.R. Mostly W.R.	WS	M. to F. Mostly M.

Depth from top in inches	Estimated % of				Consistency or induration
	Gravel	sand	silt	clay	
0-12	--	90	8	2	Squishy sand
12-30	--	100	0	0	Firm sand where undiluted

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- 4 -

Core YK-38

Depth from top in feet	% Nat. water	% Porosity	Wet Density	Rid. value	Odor	pH
0	78.00	67.5	1.57	6+	None	8.0
2	30.00	44.6	1.94	2.0	None	7.0
4	28.00	42.8	2	2.0	None	7.0
6	28.00	42.6	1.99	3.2	None	7.0
8	25.00	39.8	2	1.6	None	7.0

Description

Depth from top in inches	Color	Roundness *	Megascopic sorting**	Grain size of sand fraction***
0-12	Dark grey	S.A. to R. Mostly S.R.	S.	M. to F. Mostly M.
12-36	Medium grey salt & pepper	S.R. to W.R. Mostly W.R.	W.	M. to F. Mostly M.
36-84	Medium grey salt & pepper	S.R. to W.R. Mostly W.R.	V.P.	G. to F. Mostly M.

Depth from top in inches	Estimated % of				Consistency or induration
	Gravel	sand	silt	clay	
0-12	--	50	35	15	About like toothpaste
12-36	--	100	0	0	Very wet but firm
36-84	5	95	0	0	Very wet but firm

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Sample No. YK-16 (5'6")

Grade Size mm.	Weight	% in Grade Size	Cumulative %
>1.00	0.08	0.16	0.16
1.00-.710	0.09	0.18	0.34
.710-.500	0.15	0.30	0.64
.500-.350	0.46	0.92	1.56
.350-.250	6.78	13.60	15.16
.250-.177	16.67	33.20	48.36
.177-.125	13.88	28.70	77.06
.125-.088	5.43	10.80	87.86
.088-.062	1.18	2.40	90.26
.062-.055	0.10	0.20	90.46
.055-.031	0.70	1.40	91.86
.031-.015	0.10	0.20	92.06
.015-.009	1.00	2.00	94.06
<.009		6.30	100.36

Sample No. YK-16 (7')

>2.00	0.82	1.72	1.72
2.00-1.40	0.35	0.73	2.45
1.40-1.00	0.45	0.94	3.39
1.00-.710	0.52	1.09	4.48
.710-.500	0.73	1.53	6.01
.500-.350	1.02	2.14	8.15
.350-.250	3.34	7.00	15.15
.250-.177	5.47	11.50	26.65
.177-.125	2.70	5.66	32.31
.125-.088	1.64	3.44	35.75
.088-.062	1.40	2.94	38.69
.062-.055	1.00	2.10	40.79
.055-.031	11.00	23.00	63.79
.031-.015	4.00	8.40	72.19
.015-.009	3.80	7.90	80.09
<.009		18.00	98.09

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- 6 -

Core YK 16 Depth 5'6"

$M_d = 0.17$

$Q_1 = 0.13$

$Q_3 = 0.225$

$P_{90} = 0.07$

$P_{10} = 0.27$

Arithmetic
Parameters

$QD_a = 0.047$

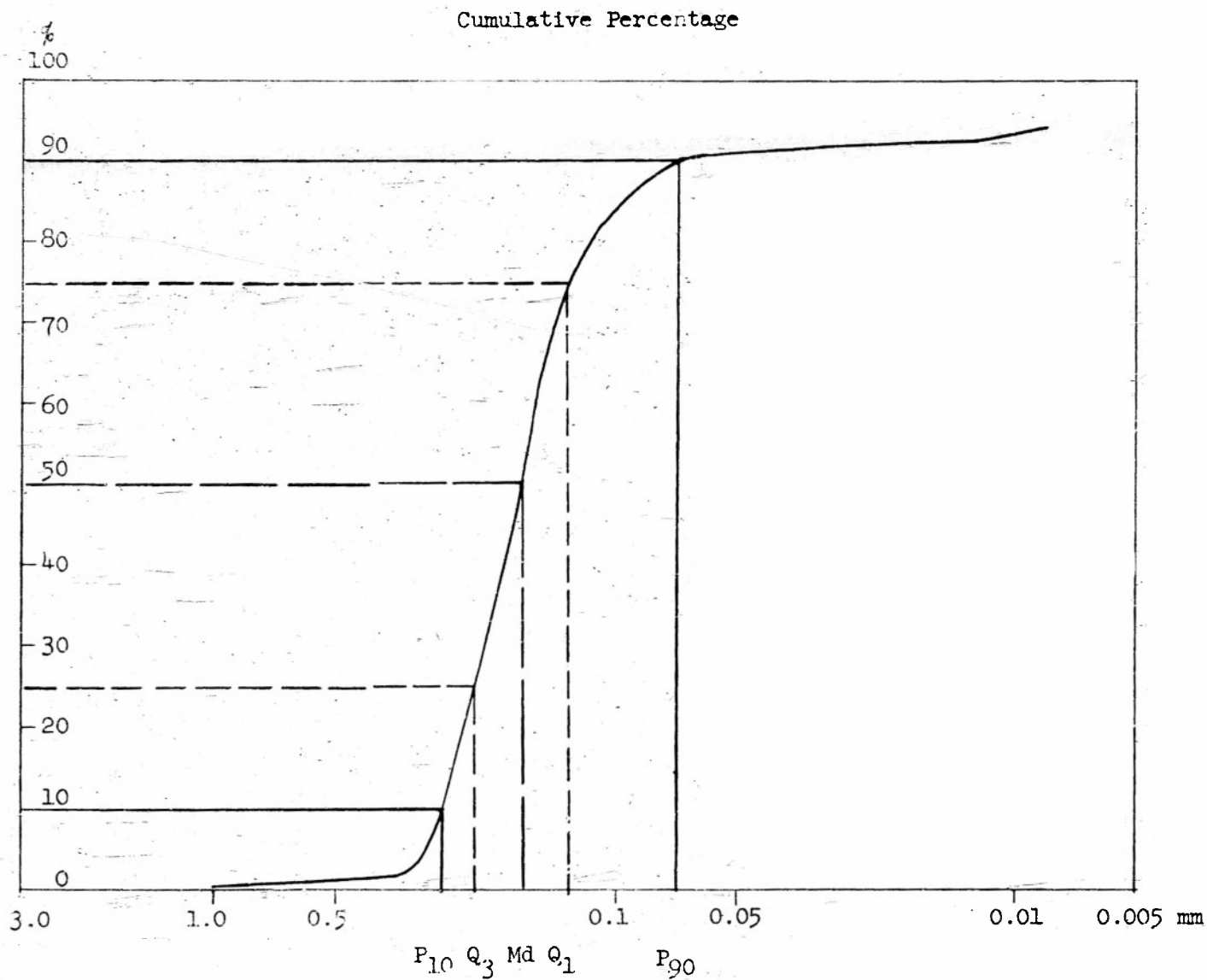
$SK_a = 0.007$

$Kq_a = -0.239$

Geometric
Parameters

$QD_g = 1.325$

$SK_g = 1.015$



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- 7 -

Core YK 16 Depth 7'

$M_d = 0.042$

$Q_1 = 0.0125$

$Q_3 = 0.185$

$P_{90} = 0.0052$

$P_{10} = 0.32$

Arithmetic
Parameters

$QD_a = 0.086$

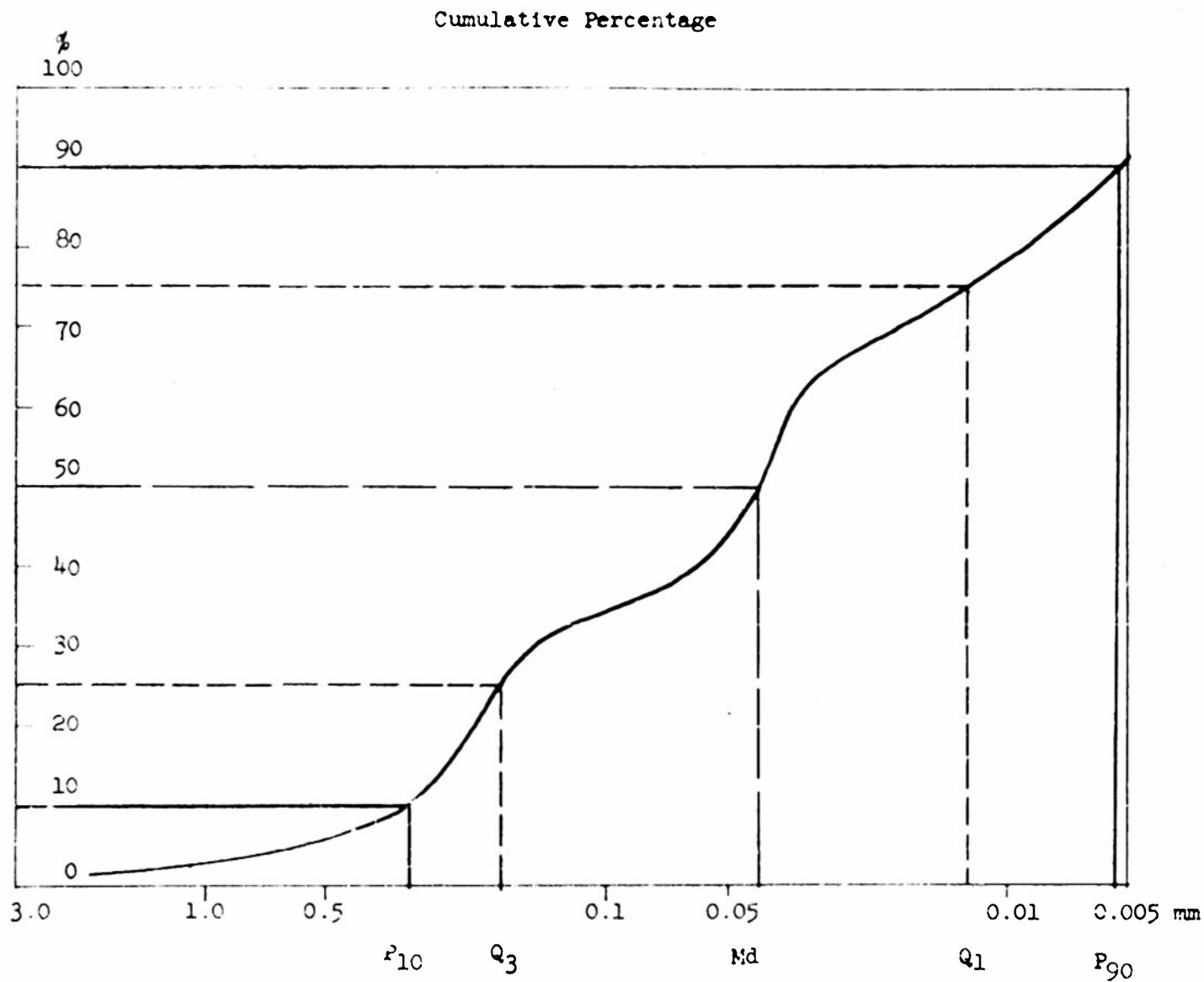
$SK_a = -0.027$

$Kq_a = -0.096$

Geometric
Parameters

$QD_g = 3.84$

$Sk = 1.34$



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- 8 -

Sample No. YK-17 (0')

Grade Size mm.	Weight	% in Grade Size	Cumulative %
>1.00	0.00	0.00	0.00
1.00-.710	0.07	0.22	0.22
.710-.500	0.08	0.25	0.47
.500-.350	0.28	0.87	1.34
.350-.250	5.32	16.40	17.74
.250-.177	2.45	7.55	25.29
.177-.125	5.72	17.60	42.89
.125-.088	2.55	7.85	50.74
.088-.062	0.52	1.60	52.34
.062-.055	1.10	3.40	55.74
.055-.031	3.00	9.30	65.04
.031-.015	3.60	11.10	76.14
.015-.009	3.30	10.20	86.34
<.009		13.60	99.94

Sample No. YK-17 (2')

>1.00	0.02	0.04	.04
1.00-.710	0.05	0.10	.14
.710-.500	0.22	0.47	.61
.500-.350	0.71	1.50	2.11
.350-.250	4.10	8.65	10.76
.250-.177	10.50	22.10	32.86
.177-.125	19.40	41.00	73.86
.125-.088	8.10	17.10	90.96
.088-.062	1.44	3.02	93.98
.062-.055	0.50	1.00	94.98
.055-.031	0.50	1.00	95.98
<.031		1.00	96.98

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- 9 -

Core YK 17 Depth 0'

Md = 0.091

Q₁ = 0.0164

Q₃ = 0.18

P₉₀ = 0.008

P₁₀ = 0.275

Arithmetic
Parameters

QD_a = 0.085

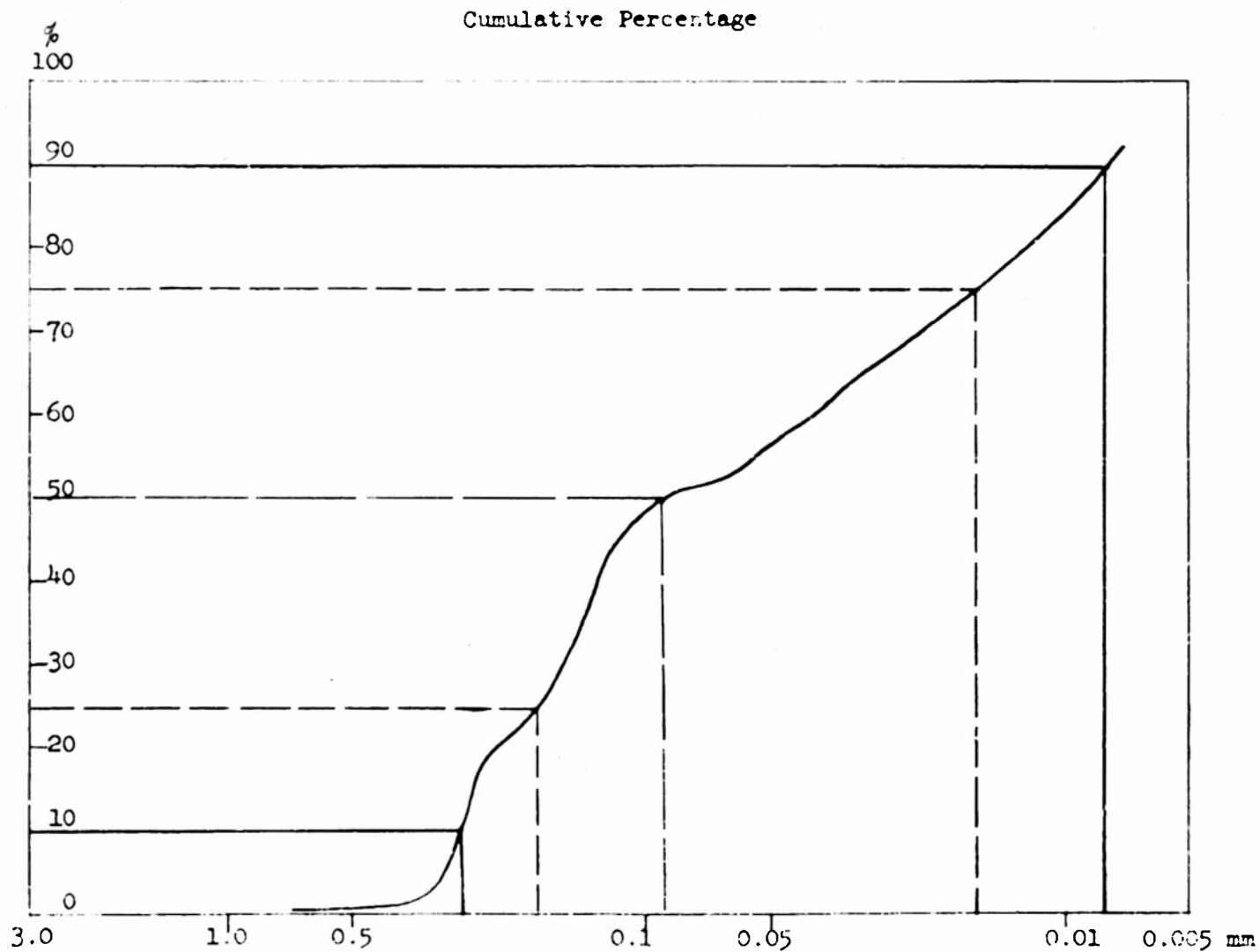
SK_a = 0.009

Kq_a = -0.318

Geometric
Parameters

QD_g = 3.34

Sk = 0.035



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- 10 -

Core YK 17 Depth 2'

$M_d = 0.155$

$Q_1 = 0.12$

$Q_3 = 0.19$

$P_{90} = 0.089$

$P_{10} = 0.25$

Arithmetic
Parameters

$QD_a = 0.035$

$SK_a = 0.0$

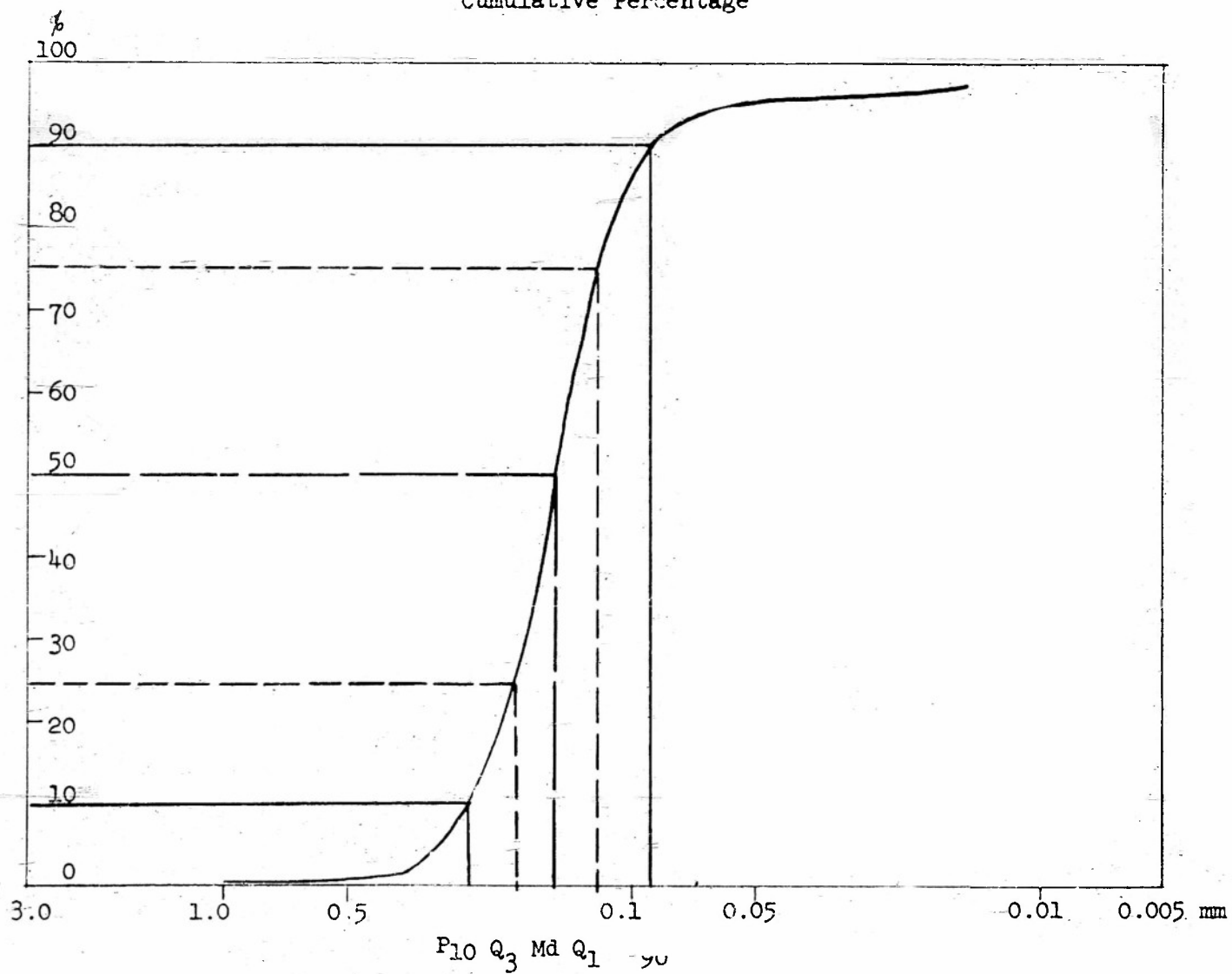
$Kq_a = -0.217$

Geometric
Parameters

$QD_g = 1.259$

$Sk = 0.949$

Cumulative Percentage



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Sample No. YK-18 (0')

Grade Size mm.	Weight	% in Grade Size	Cumulative %
>2.00	0.00	0.00	0.00
2.00-1.40	0.00	0.00	0.00
1.40-1.00	0.00	0.00	0.00
1.00-.710	0.06	0.20	0.20
.710-.500	0.06	0.20	0.40
.500-.350	0.10	0.32	0.72
.350-.250	0.31	1.00	1.72
.250-.177	0.62	2.00	3.72
.177-.125	1.05	3.36	7.08
.125-.088	3.26	10.40	17.48
.088-.062	6.55	20.90	38.38
.062-.055	5.40	17.30	55.68
.055-.031	6.00	19.20	74.88
.031-.015	2.30	7.35	82.23
.015-.009	4.30	13.75	95.98
<.009	1.30	4.15	100.13

Sample No. YK-18 (4')

>2.00	0.20	0.43	0.43
2.00-1.40	0.20	0.43	0.43
1.40-1.00	0.26	0.56	1.25
1.00-.710	0.34	0.73	1.98
.710-.500	0.80	1.73	3.71
.500-.350	1.60	3.40	7.11
.350-.250	19.32	43.00	50.11
.250-.177	4.35	9.40	59.51
.177-.125	9.44	20.20	79.71
.125-.088	1.76	3.80	83.51
.088-.062	0.28	0.60	84.11
.062-.055	0.13	0.27	84.38
.055-.031	0.75	1.50	85.88
.031-.015	0.75	1.50	87.38
.015-.009	1.40	2.80	90.18
<.009	0.50	1.00	91.18
	0.50	8.70	99.88

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- 12 -

Core YK 18 Depth 0'

$$M_d = 0.058$$

$$Q_1 = 0.031$$

$$Q_3 = 0.076$$

$$P_{90} = 0.0105$$

$$P_{10} = 0.19$$

Arithmetic
Parameters

$$QD_a = 0.022$$

$$SK_a = -0.005$$

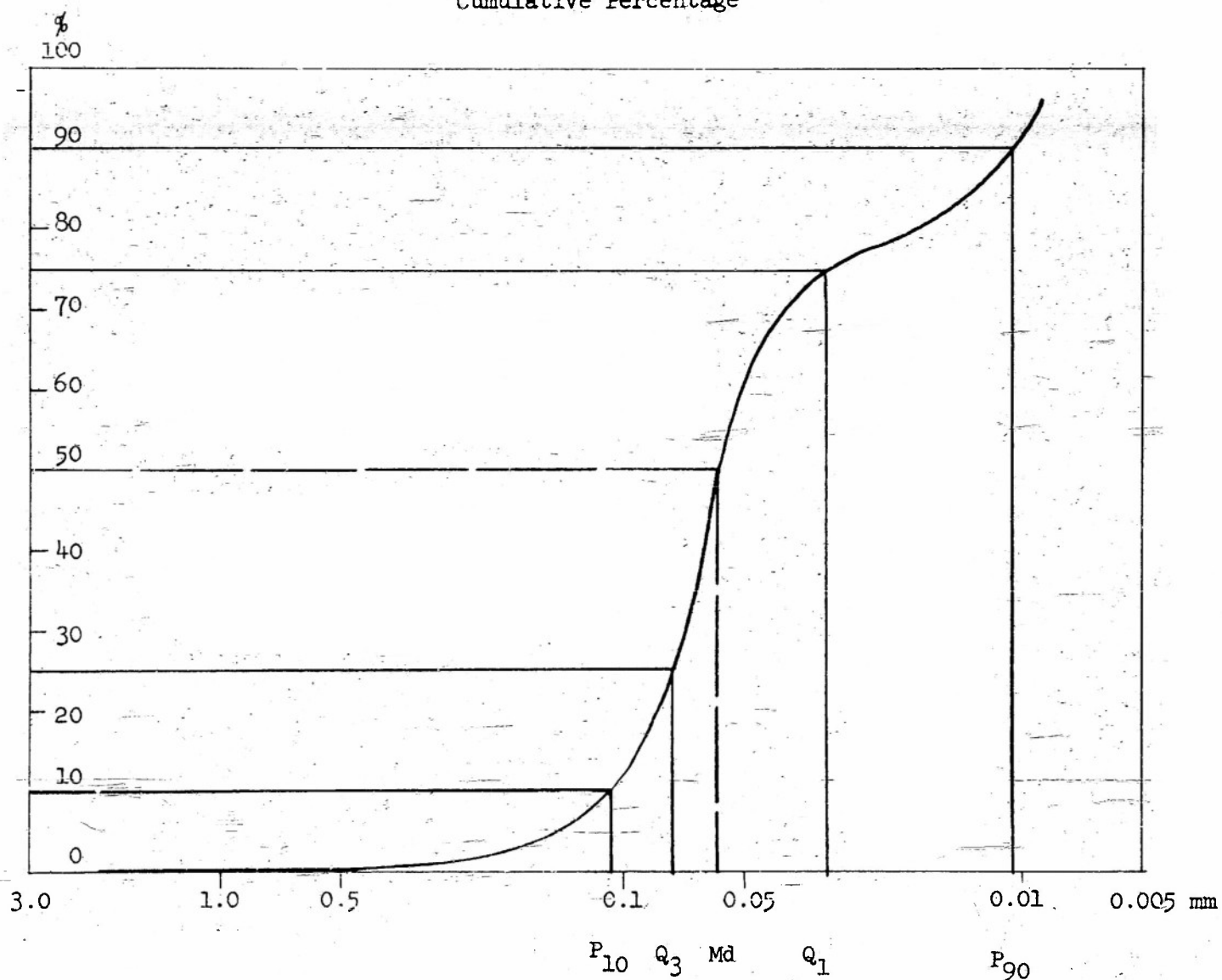
$$KQ_a = -0.125$$

Geometric
Parameters

$$QD_g = 1.565$$

$$SK_g = 0.792$$

Cumulative Percentage



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- 13 -

Core YK 18 Depth 4'

Md = 0.20

Q₁ = 0.14

Q₃ = 0.26

P₉₀ = 0.017

P₁₀ = 0.33

Arithmetic
Parameters

QD_a = 0.06

SK_a = 0.0

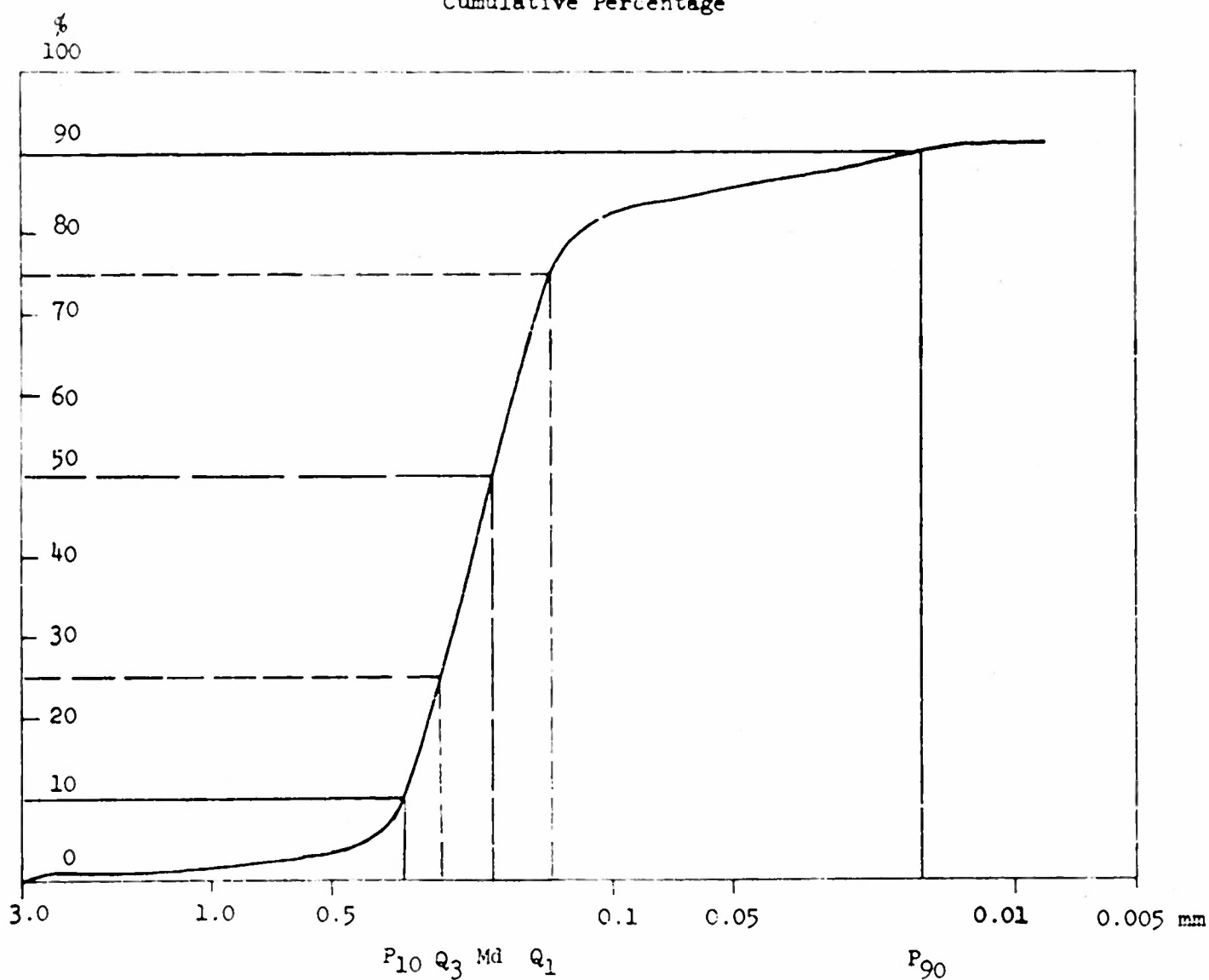
K_q_a = -0.192

Geometric
Parameters

QD_g = 1.36

Sk = 0.909

Cumulative Percentage



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Sample No. YK-18 (6')

Grade Size mm.	Weight	% in Grade Size	Cumulative %
>2.00	0.08	0.20	0.20
2.00-1.40	0.07	0.17	0.37
1.40-1.00	0.14	0.34	0.71
1.00-.710	0.18	0.45	1.16
.710-.500	0.30	0.75	1.91
.500-.350	0.50	1.25	3.16
.350-.250	1.18	2.94	6.10
.250-.177	1.85	4.61	10.71
.177-.125	1.43	3.56	14.27
.125-.088	2.83	7.05	21.32
.088-.062	5.42	13.50	34.82
.062-.055	3.60	9.00	43.82
.055-.031	8.10	21.00	64.82
.031-.015	4.20	10.50	75.32
.015-.009	4.80	12.00	87.32
<.009	5.40	13.00	100.32

Sample No. YK-36 (0')

>2.00	0.07	0.22	0.22
2.00-1.40	0.00	0.00	0.22
1.40-1.00	0.04	0.13	0.35
1.00-.710	0.04	0.13	0.48
.710-.500	0.04	0.13	0.61
.500-.350	0.04	0.13	0.74
.350-.250	0.15	0.48	1.22
.250-.177	0.24	0.77	1.99
.177-.125	0.37	1.18	3.17
.125-.088	0.42	1.34	4.51
.088-.062	0.39	1.25	5.76
.062-.055	1.00	3.20	8.96
.055-.031	3.00	9.50	18.46
.031-.015	4.70	14.90	33.36
.015-.009	5.40	17.20	50.56
<.009		47.60	98.16

CONFIDENTIAL

- 15 -

Core YK 18 Depth 6'

$M_d = 0.048$

$Q_1 = 0.015$

$Q_3 = 0.078$

$P_{90} = 0.0036$

$P_{10} = 0.18$

Arithmetic
Parameters

$QD_a = 0.033$

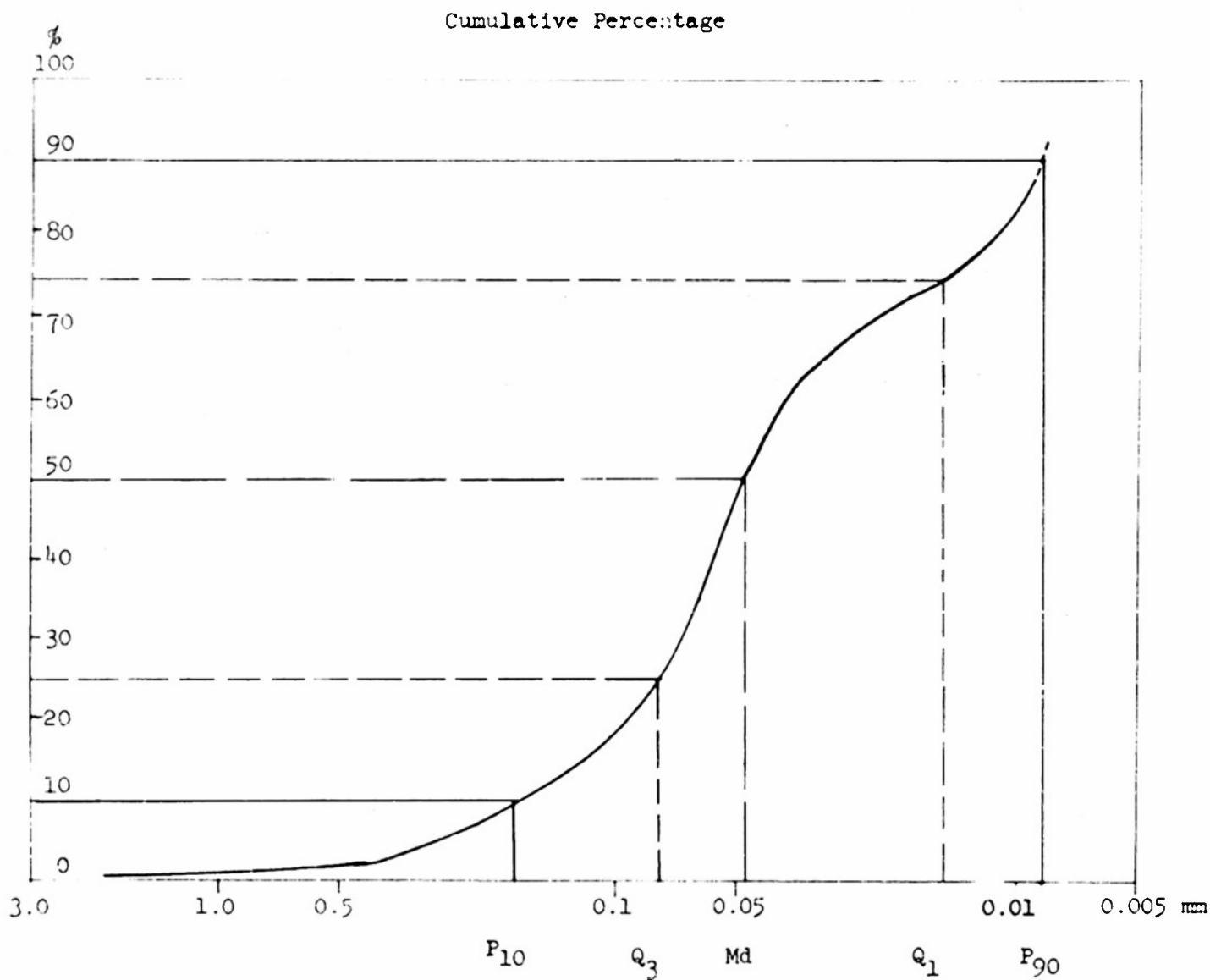
$SK_a = -0.01$

$Kq_a = -0.184$

Geometric
Parameters

$QD_g = 2.28$

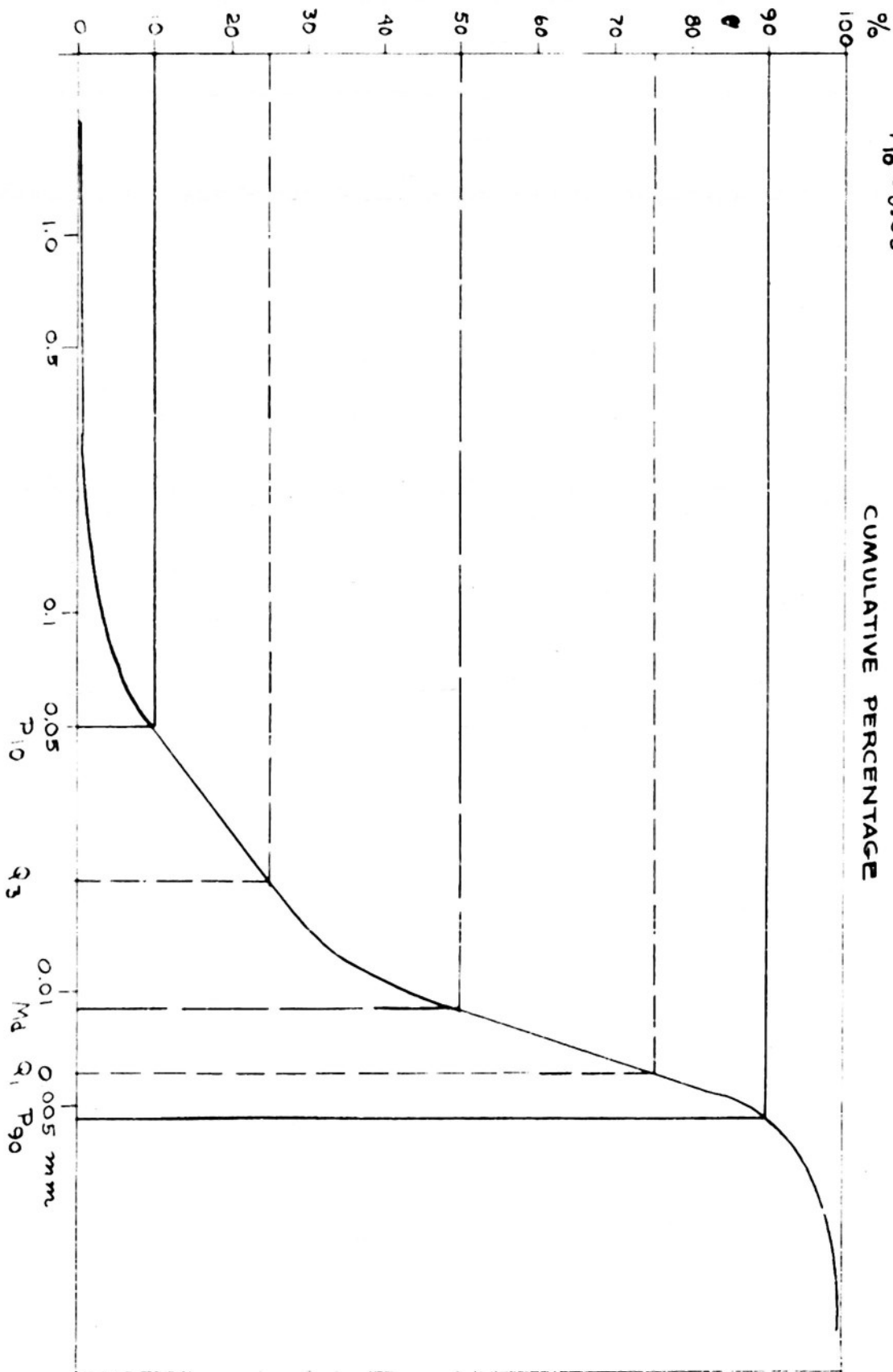
$Sk = 0.518$



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- 16 -



Md = .009
Q₁ = 0.006
Q₃ = 0.019
P₉₀ = 0.0046
P₁₀ = 0.05

CORE YK 36 (0')

Arithmetic Parameters
QD_a = 0.006
SK_a = 0.006
K_{ga} = -0.144

Geometric Parameters
QD_g = 1.78
SK = 1.40

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Sample No. YK-36 (5')

Grade Size mm.	Weight	% in Grade Size	Cumulative %
1.40-1.00	0.11	0.22	0.22
1.00-.710	0.15	0.31	0.53
.710-.500	0.19	0.39	0.92
.500-.350	0.41	0.84	1.76
.350-.250	7.00	14.30	16.06
.250-.177	15.45	31.50	47.56
.177-.125	15.14	30.90	78.46
.125-.088	5.24	10.70	89.16
.088-.062	1.11	2.26	91.42
.062-.055	0.10	0.20	91.62
.055-.031	0.30	0.60	92.22
.031-.015	0.30	0.60	92.82
.015-.009	0.50	1.00	93.82
<.009		5.80	99.62

Sample No. YK-37 (0')

>2.00	0.89	1.87	1.87
2.00-1.40	0.11	0.23	2.10
1.40-1.00	0.22	0.46	2.56
1.00-.710	0.17	0.36	2.92
.710-.500	0.30	0.63	3.55
.500-.350	0.58	1.22	4.77
.350-.250	7.50	15.80	20.57
.250-.177	17.03	35.80	56.37
.177-.125	9.74	20.40	76.77
.125-.088	4.52	9.50	86.27
.088-.062	1.09	2.30	88.57
.062-.055	1.00	2.10	90.67
.055-.031	0.10	0.21	90.88
.031-.015	0.00	0.00	90.88
.015-.009	0.90	1.90	92.78
<.099		6.50	99.28

CONFIDENTIAL

- 18 -

Core YK 36 Depth 5'

$$M_d = 0.155$$

$$Q_1 = 0.132$$

$$Q_3 = 0.215$$

$$P_{90} = 0.08$$

$$P_{10} = 0.275$$

Arithmetic
Parameters

$$QD_a = 0.04$$

$$SK_a = 0.018$$

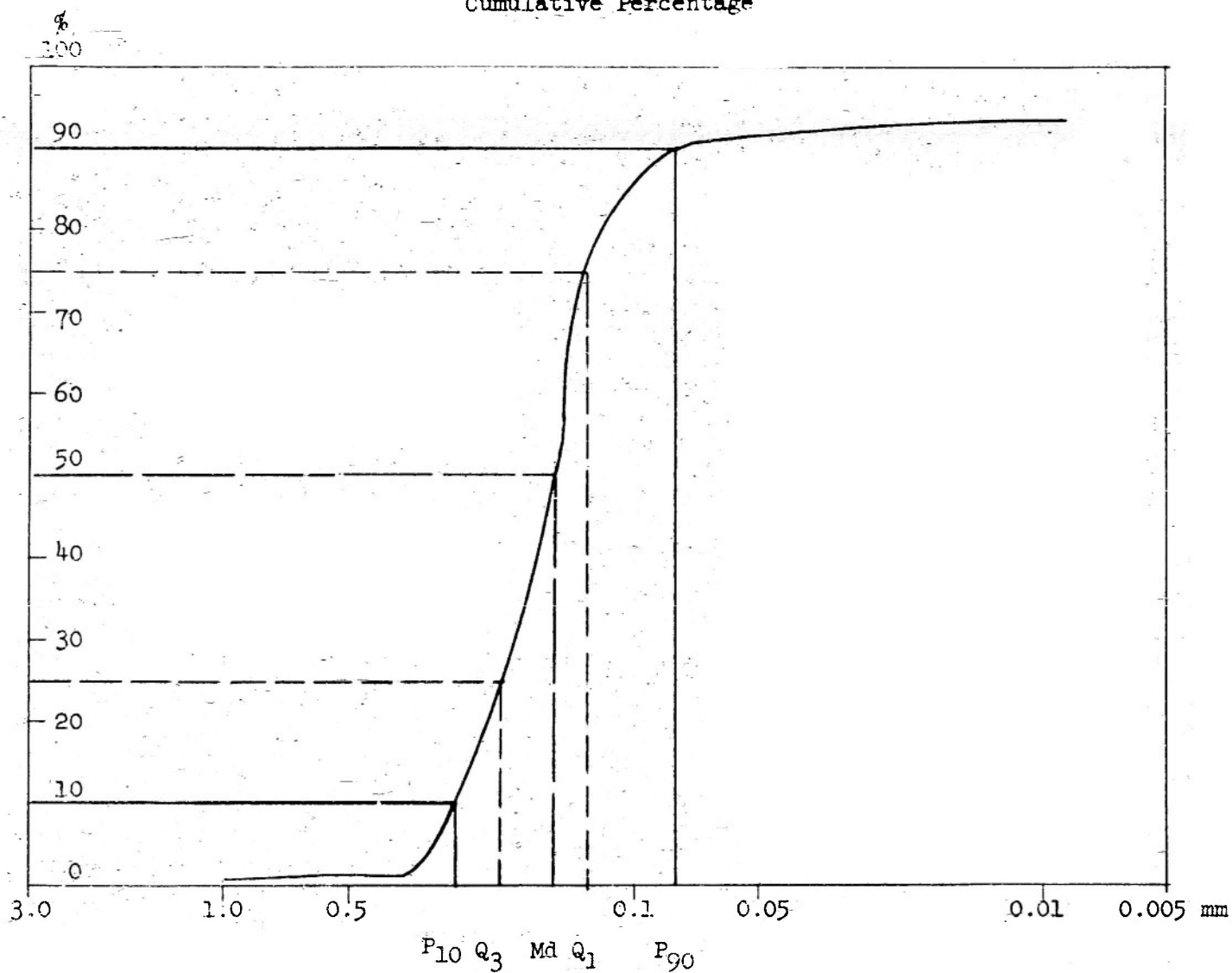
$$Kq_a = -0.205$$

Geometric
Parameters

$$QD_g = -1.259$$

$$SK = 1.225$$

Cumulative Percentage



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- 19 -

Core YK 37 Depth 0'

$$M_d = 0.182$$

$$Q_1 = 0.135$$

$$Q_3 = 0.235$$

$$P_{90} = 0.046$$

$$P_{10} = 0.29$$

Arithmetic
Parameters

$$QD_a = 0.05$$

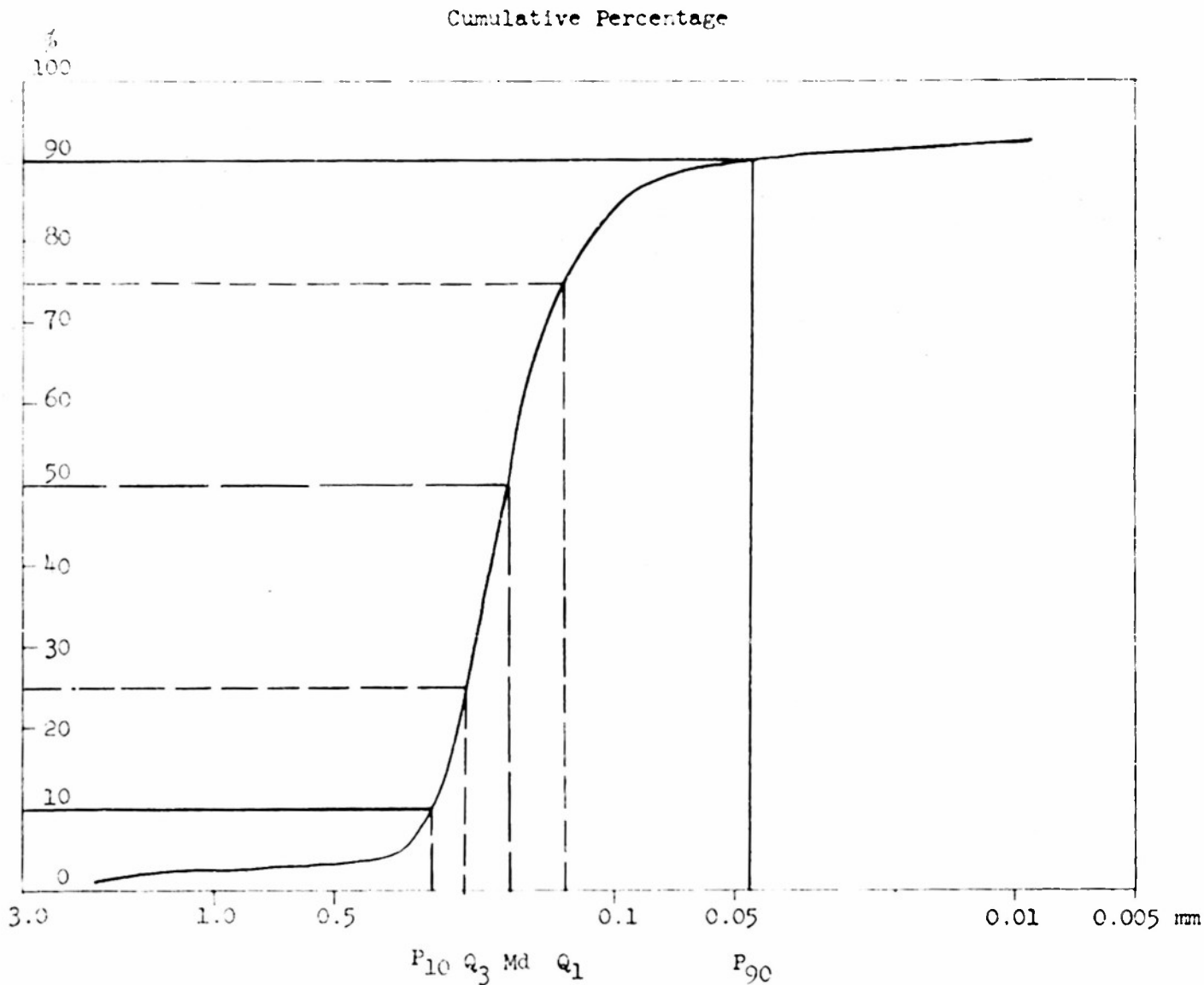
$$SK_a = 0.003$$

$$Kq_a = -0.397$$

Geometric
Parameters

$$QD_g = 1.318$$

$$Sk = 0.96$$



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Sample No. YK-37 (2'6")

Grade Size mm.	Weight	% in Grade Size	Cumulative %
>1.00	0.00	0.00	
1.00-.710	0.02	0.05	.05
.710-.500	0.12	0.25	.30
.500-.350	0.37	0.82	1.12
.350-.250	4.68	10.50	11.62
.250-.177	15.51	35.00	46.62
.177-.125	15.63	35.00	81.62
.125-.088	5.04	11.30	92.92
.088-.062	1.34	3.00	95.92
.062-.055	0.20	0.45	96.37
.055-.031	0.20	0.45	96.82
.031-.015	0.20	0.45	97.27
.015-.009	0.20	0.45	97.72
<.009		0.90	98.62

Sample No. YK-38 (0')

>2.00	0.01	0.02	0.02
2.00-1.40	0.00	0.00	0.02
1.40-1.00	0.01	0.02	0.04
1.00-.710	0.05	0.12	0.16
.710-.500	0.11	0.25	0.41
.500-.350	0.43	1.00	1.41
.350-.250	3.24	7.50	8.91
.250-.177	10.48	24.30	33.21
.177-.125	10.20	23.70	56.91
.125-.088	5.76	13.40	70.31
.088-.062	3.26	7.55	77.86
.062-.055	1.70	3.90	81.76
.055-.031	1.50	3.50	85.26
.031-.015	1.30	3.00	88.26
.015-.009	1.00	2.30	90.56
<.009		4.80	95.36

CONFIDENTIAL

- 21 -

Core YK 37 Depth 2'6"

$$M_d = 0.17$$

$$Q_1 = 0.135$$

$$Q_3 = 0.21$$

$$P_{90} = 0.1$$

$$P_{10} = 0.25$$

Arithmetic
Parameters

$$QD_a = 0.037$$

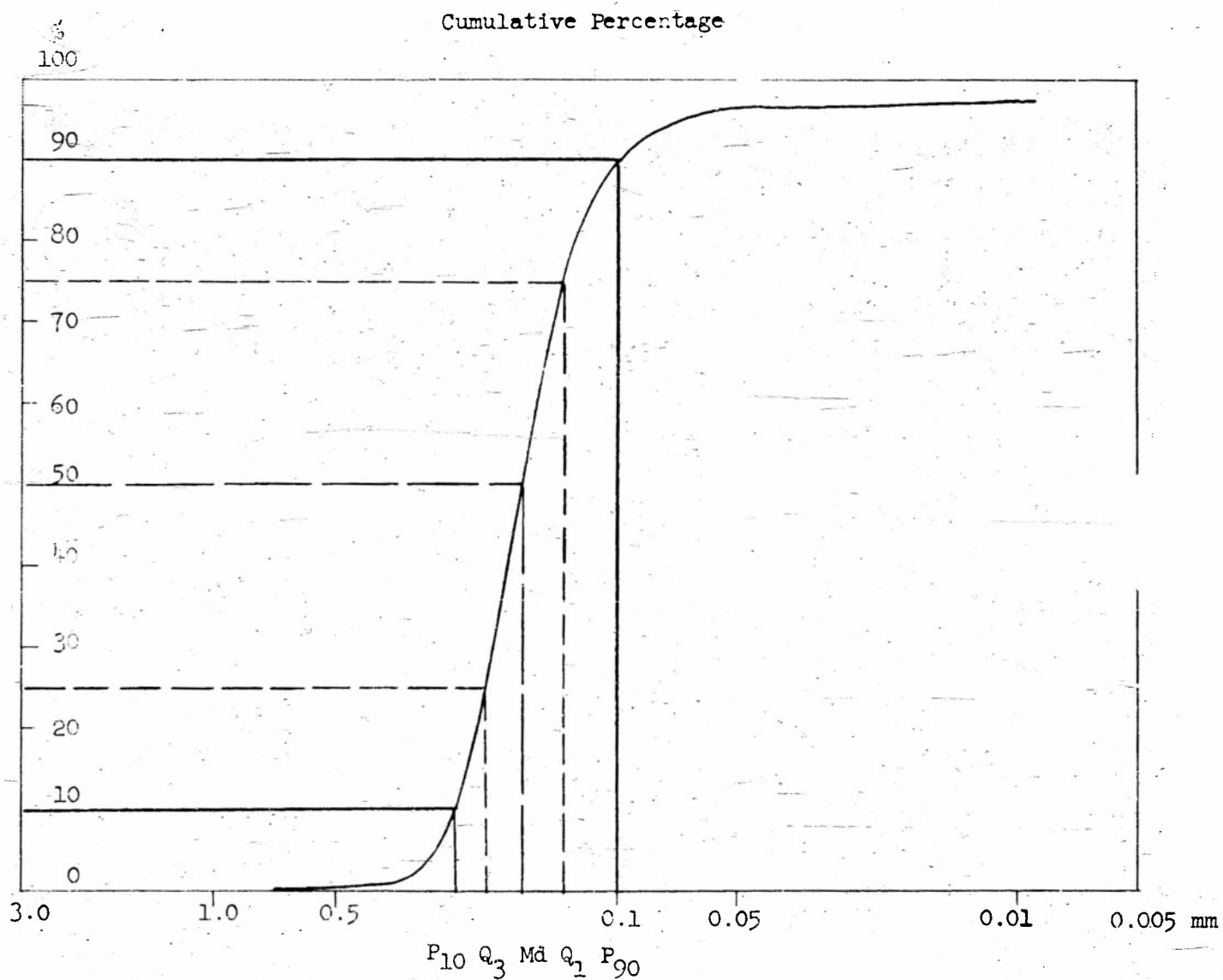
$$SK_a = 0.007$$

$$Kq_a = -0.25$$

Geometric
Parameters

$$QD_g = 1.245$$

$$SK = 0.98$$



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- 22 -

Core YK 38 Depth 0'

$M_d = 0.14$

$Q_1 = 0.072$

$Q_3 = 0.19$

$P_{90} = 0.01$

$P_{10} = 0.24$

Arithmetic
Parameters

$QD_a = 0.06$

$SK_a = 0.12$

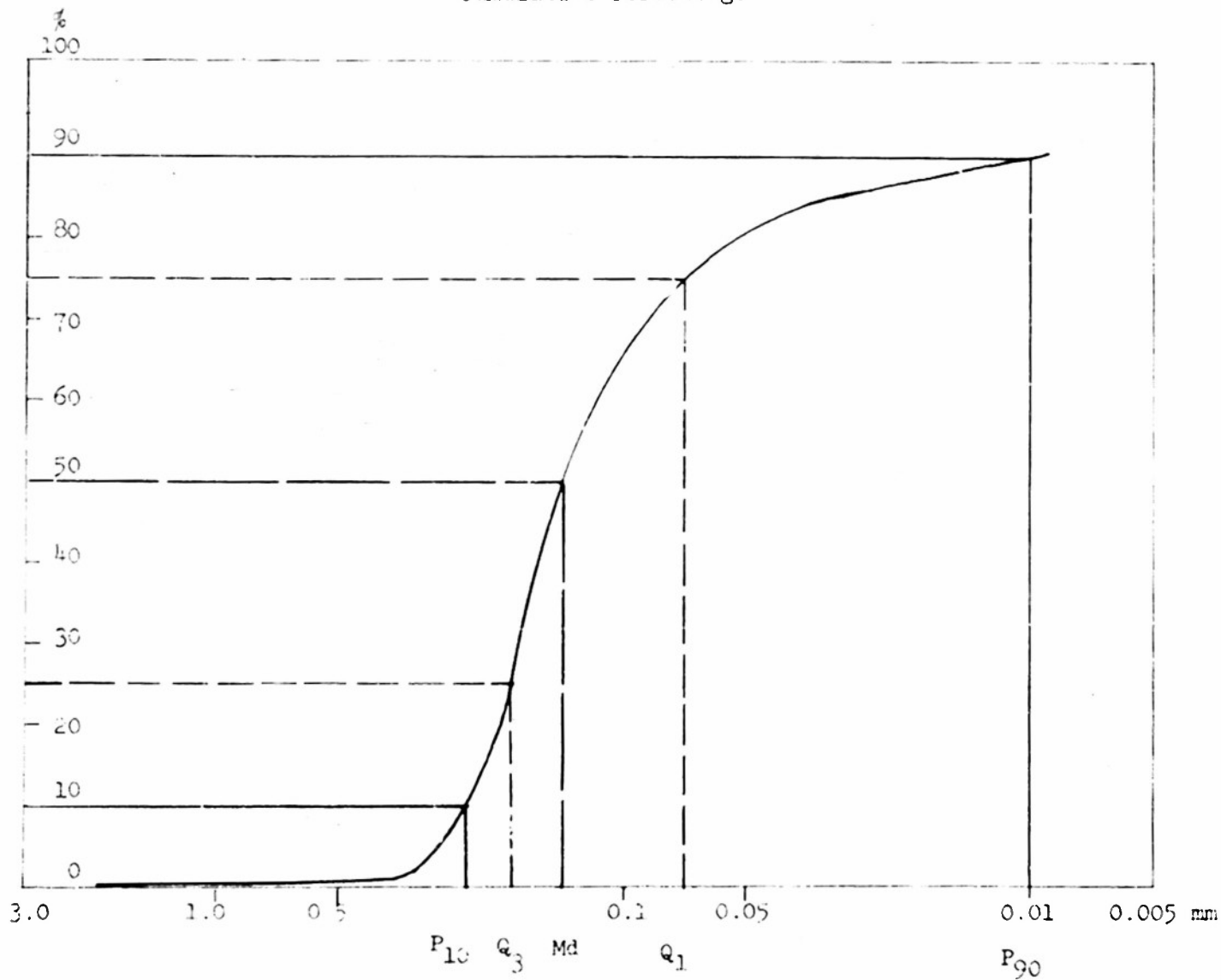
$Kq_a = -0.261$

Geometric
Parameters

$QD_g = 1.645$

$SK = 0.694$

Cumulative Percentage



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Sample No. YK-38 (1'6")

Grade Size mm.	Weight	% in Grade Size	Cumulative %
>2.00	0.31	0.62	0.62
2.00-1.40	0.25	0.50	1.12
1.40-1.00	0.47	0.94	2.06
1.00-.710	0.73	1.46	3.52
.710-.500	1.18	2.36	5.88
.500-.350	2.15	4.31	10.19
.350-.250	8.55	17.10	27.29
.250-.177	13.80	27.60	54.89
.177-.125	14.68	29.20	84.09
.125-.088	4.92	9.85	93.94
.088-.062	0.94	1.88	95.82
.062-.055	0.20	0.40	96.22
.055-.031	0.30	0.60	96.82
.031-.015	0.50	1.00	97.82
.015-.009	0.40	0.80	98.62
<.009		2.60	101.22

Sample No. YK-38 (5')

>2.00	5.48	11.18	11.10
2.00-1.40	1.07	2.18	13.28
1.40-1.00	1.20	2.34	15.62
1.00-.710	1.37	2.78	18.40
.710-.500	2.13	4.34	22.74
.500-.350	3.30	6.70	29.44
.350-.250	6.80	13.80	43.24
.250-.177	7.78	15.80	59.04
.177-.125	11.64	23.70	82.74
.125-.088	4.02	8.15	90.89
.088-.062	1.00	2.02	92.91
.062-.055	0.30	0.60	93.51
.055-.031	0.50	1.00	94.51
.031-.015	0.30	0.60	95.11
.015-.009	0.55	1.20	96.31
<.009		3.60	99.91

CONFIDENTIAL

- 24 -

Core YK 38 Depth 1'6"

$$M_d = 0.19$$

$$Q_1 = 0.14$$

$$Q_3 = 0.26$$

$$P_{90} = 0.11$$

$$P_{10} = 0.37$$

Arithmetic
Parameters

$$QD_a = 0.06$$

$$SK_a = 0.01$$

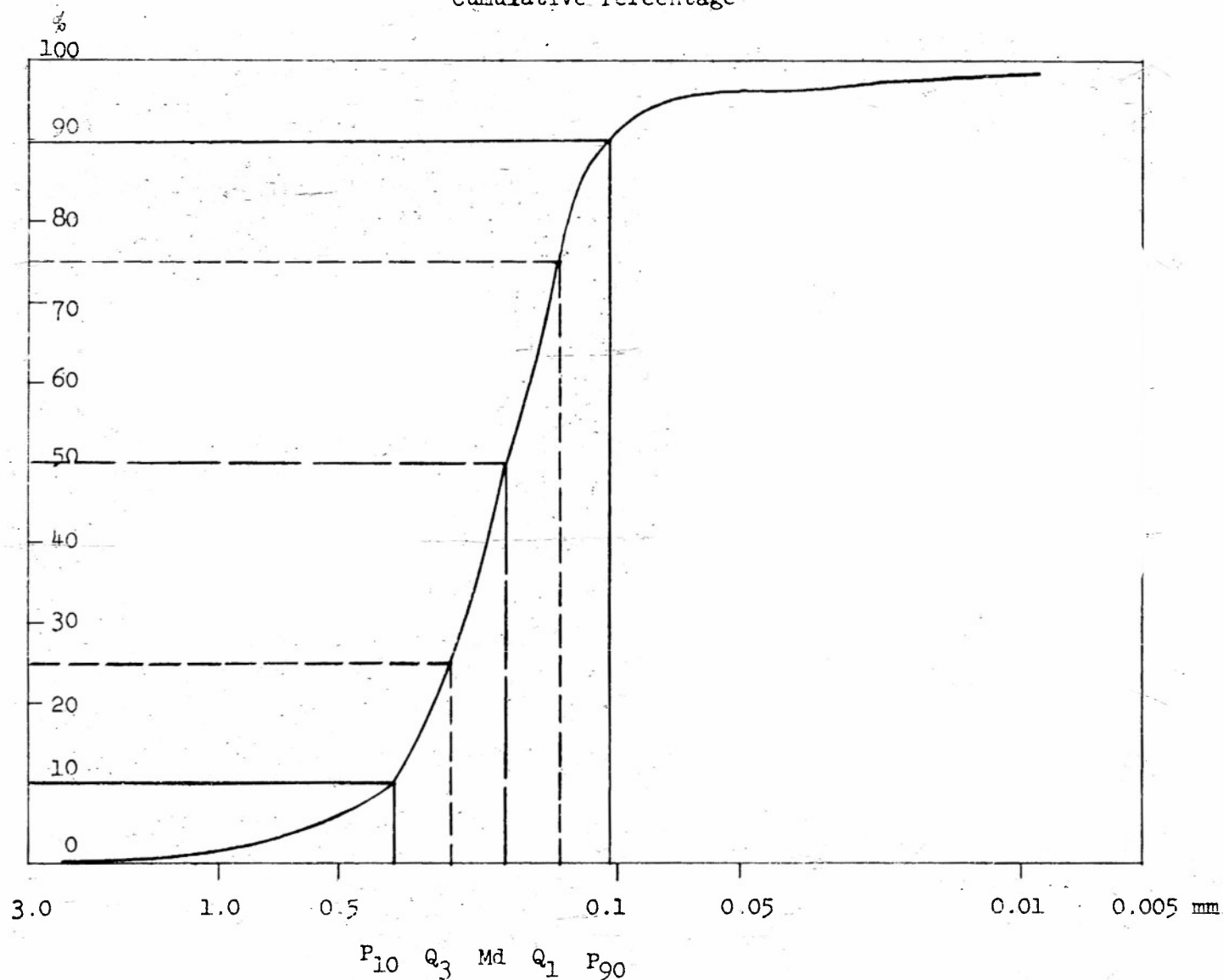
$$Kq_a = -0.231$$

Geometric
Parameters

$$QD_g = 1.36$$

$$Sk = 1.01$$

Cumulative Percentage



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- 25 -

Core YK 38 Depth 5'

$$Md = 0.21$$

$$Q_1 = 0.137$$

$$Q_3 = 0.43$$

$$P_{90} = 0.092$$

$$P_{10} = 2.7$$

Arithmetic
Parameters

$$QD_a = 0.146$$

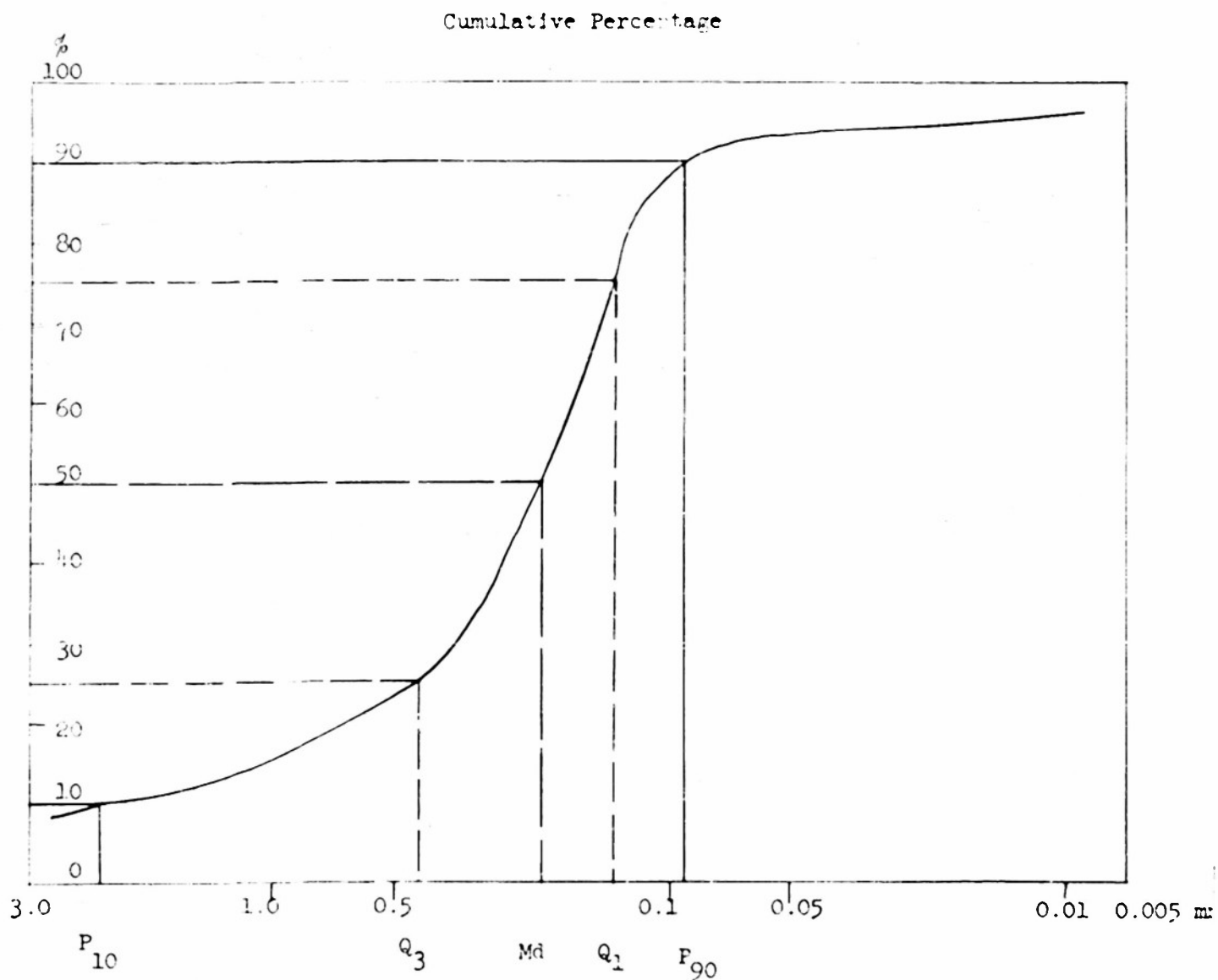
$$SK_a = 0.073$$

$$Kq_a = -0.056$$

Geometric
Parameters

$$QD_g = 1.77$$

$$Sk = 1.33$$



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